Progress Report

March 2, 2016 Steam Enhanced Extraction at the Former Williams AFB, ST012 Site

Mesa, AZ



1. Summary

This report covers the period of operations from Tuesday, February 23, 2016 through Monday, February 29, 2016. The following table provides a summary of the project operational status.

Table 1. Project Summary

Table 21 11 oject Sammar y		
	Value	Unit
Target Treatment Zone (TTZ) Soil Volume	410,000	cubic yards (cy)
Area	199,000	square feet (ft²)
Upper Depth of Treatment	145	feet (ft) below ground surface (bgs)
Lower Depth of Treatment	245	ft bgs
Vapor Liquid Treatment Started	09/29/14	
Thermal Operations Started	09/29/14	
Last Process Data Update	02/29/16	
Last Temperature Data Update	02/29/16	
Estimated Total Days of Operation	422	days
Days of Operation	518	days
Days of Operation vs. Estimate	123	percent (%)
Estimated Total Energy Usage	11,343,000	kilowatt hours (kWh)
Total Energy Used	5,333,263	kWh
Used Electrical Energy vs. Estimate	47	%
Total Steam Injected	299.5	million pounds (lbs)
Projected Total Steam Injection	320	million lbs
Steam Injected Vs Projected	94	%
Total Mass Removed in Vapor Based on		
Photoionization Detector (PID) Readings	1,103,281	lbs
Total Mass Removed as NAPL	1,335,733	lbs
Average Daily NAPL Mass Removal Last Week	1,343	lbs/day
Total Vapor and Liquid Mass Removal (based on		lbs
PID readings)	2,439,014	103
Average Power Usage Rate Last Week	526	kilowatts (kW)
Average Wellfield Vapor Extraction Rate Last	439	standard cubic feet per minute (scfm)
Average Condensate Production Rate Last Week	0.7	gallons per minute (gpm)
Average Water Extraction Rate Last Week	161	gpm
Total Water Extracted	83,241,748	gallons
Total Recovered Light Non-Aqueous Phase Liquid	203,308	gallons
Average Water Discharge Rate Last Week	200	gpm
Total Treated Water Discharge	110,963,000	gallons

Operational highlights from the past week include:

- Steam injection was restarted on Thursday, February 18, 2016 following the site wide depressurization on February 5, 2016.
- The second air stripper blower and motor were reinstalled and the second air stripper was restarted on Tuesday, February 23, 2016. Both air strippers are now operating.
- The average total steam injection rate for this period was 34,700 lbs/hr or 69.5 gpm;
 9,100 lbs/hr (18.2 gpm) in the Cobble Zone (CZ), 15,500 lbs/hr (31.0 gpm) in the Upper Water Bearing Zone (UWBZ), and 10,100 lbs/hr (20.2 gpm) in the Lower Saturated Zone (LSZ).
- The average liquid extraction rate from the formation was approximately 161 gpm (2.3 times the injection rate).
- Collected process, wellfield and laboratory samples per the sampling schedule.
- Conducted regular maintenance on the treatment system.
- The following MPE wells will require maintenance:
 - o CZ08*
 - o CZ11*

^{*}Temperatures at these MPE wells are at boiling – well maintenance will be postponed until temperatures are below boiling due to health and safety concerns.

2. Vapor Extraction

Figure 1 below shows the vapor extraction rate from the site. Note that the estimated steam extraction rate is a calculated value based on the water generated at the moisture separators after cooling the vapors from the wellfield. Based on energy balance analysis, additional steam is likely being pulled into and condensing in the liquid extraction system. This steam extraction is not measureable and not accounted for in Figure 1. Additionally the wellfield flow is calculated as the difference between the air stripper flows and thermal accelerator influent, and is therefore only an estimate.

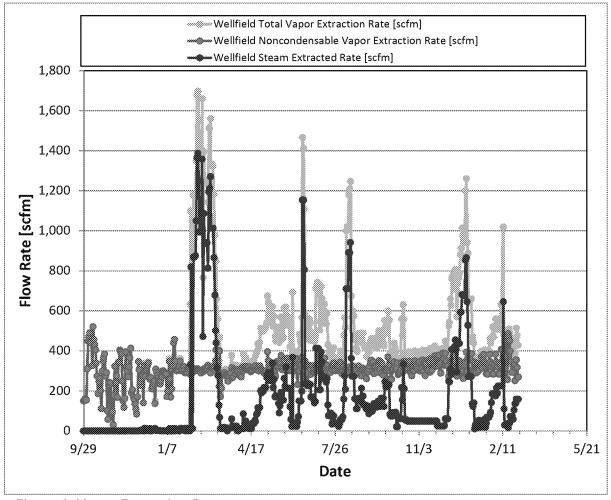


Figure 1. Vapor Extraction Rate

Note: Well SVE01M was tied into the SEE extraction system on June 5, 2015. Wells SVE10M and SVE14M were tied into the SEE extraction system on September 23, 2015.

3. PID Measurements

The following figure depicts the PID concentrations from the wellfield effluent to the effluent of the thermal accelerators collected since the start of operations. Note that PID readings of 0.0 parts per million by volume (ppmV) are shown in the figures as 0.01 ppmV due to the logarithmic scale that does not allow display of 0-values. Accelerator influent readings are interpolated for days where no data is collected, since the value is used in the mass removal calculation.

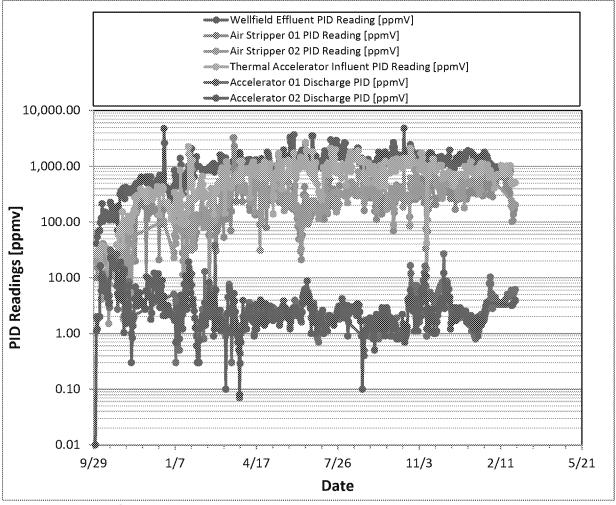


Figure 2. PID Readings

4. Mass Removal

The mass removal is calculated based on the PID and laboratory data collected at the thermal accelerator influent and the LNAPL recovered. The figure also depicts the mass removed based on PID and laboratory data.

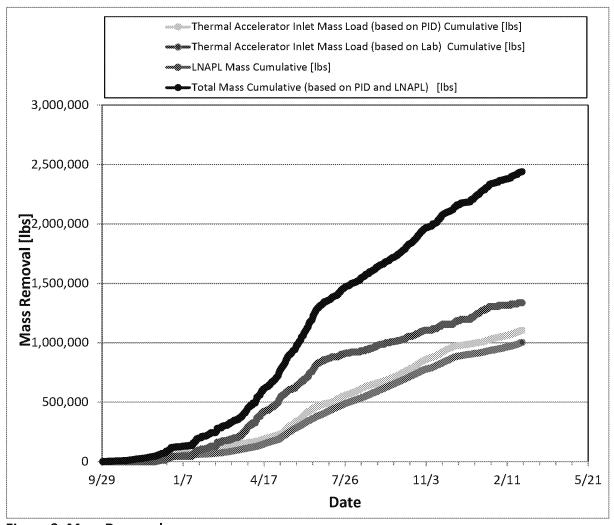


Figure 3. Mass Removal

Note: A NAPL density of 6.57 lbs/gallons is used to convert the NAPL volume to pounds. A molecular weight of 106,168 g/mol (corresponding to xylene) is used to convert PID readings to concentrations.

5. Daily Mass Removed

Figure 4 outlines the daily mass removed as vapor and LNAPL. The total daily mass removed is the combination of vapor and LNAPL. The liquid mass removal is captured in the vapor phase due to the volatilization of liquid contaminants in the air strippers.

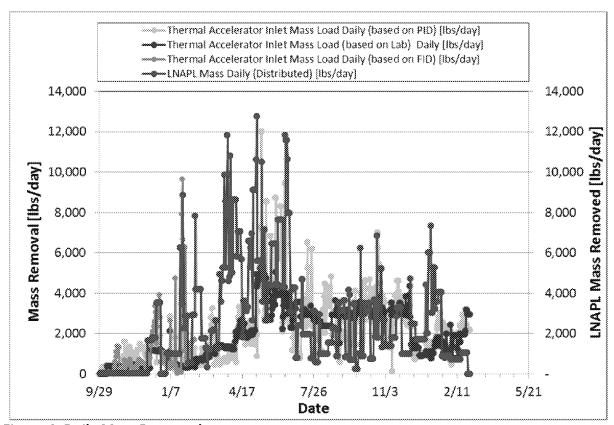


Figure 4. Daily Mass Removed

Note: Laboratory data are not collected daily. The "Thermal Accelerator Inlet Mass Load (based on lab)" is an average daily rate of actual lab data collected. The report has been updated based on lab data received for samples collected through January 11, 2016.

Note that accumulated LNAPL is pumped through the NAPL conditioning system in a batch style process. The LNAPL daily mass removal rate has been calculated by calculating an average daily rate based on the total gallons processed for each batch over the number of days between batches.

6. Power Usage

The cumulative power usage is shown below. All electricity used at the site is utilized to run the process system and steam generators.

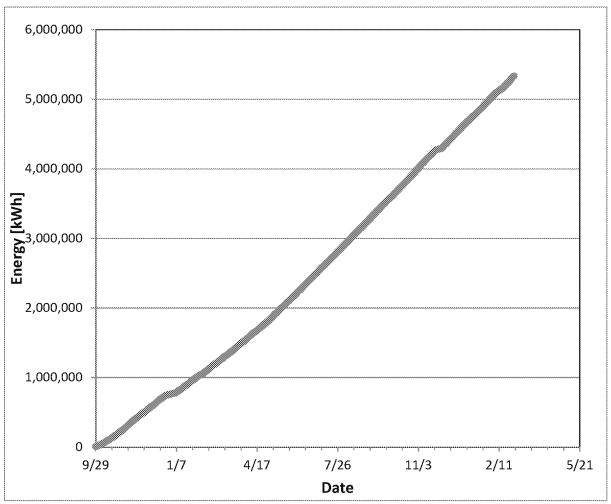


Figure 5. Cumulative Power Usage

7. Average Temperature

A detailed review of thermocouple sensor depths and temperatures over time was performed week ending November 13, 2015. Results of the review and updates are detailed below in Table 2 and Figure 6.

Table 2. Temperature Monitoring Sensor History

Temperature Monitoring Point	Temperature Monitoring Sensor History
TMP01	Well compromised 6/9/2015, select sensors back online 7/15/2015. Well not extended down in the Lower Permeable Zone (LPZ) and LSZ.
TMP03	Well compromised 12/18/15. All sensors offline as of 12/18/15.
TMP04	Well compromised 6/21/2015. Not included in LPZ and LSZ since 6/21/2015.
TMP05	Well compromised 5/6/2015, select sensors back online 7/15/2015. Sensors deeper than 160 ft have not been online since 5/6/2015 and therefore are not included in UWBZ, LPZ and LSZ.
TMP06	Well compromised 3/27/2015, select sensors back online 7/14/2015.
TMP07	Well compromised 3/27/2015, select sensors back online 7/14/2015.
TMP08	Well partly compromised 9/11/2015 from 210 ft and down. The 215 and 235 ft sensors are still operating.
TMP09	Well compromised 2/9/2015 before CZ was turned on and UWBZ was up to temperature. The CZ and UWBZ temperatures have been excluded. LSZ temperatures have not been updated since 2/9/2015 (taken out of LSZ average).
TMP12	Sensors from 150 to 170 ft bgs only at $^{\sim}50$ C. Brings down the average in CZ and UWBZ.
TMP13	Well compromised 3/27/2015, select sensors back online 4/30/2015. Since 7/1/2015 no sensor deeper than 225 ft has been operational.
TMP15	Well compromised 8/15/2015. 8/15/2015 temperatures assumed from this day.
TMP17	Well compromised 3/27/2015, select sensors back online 6/12/2015 but not reporting properly, total failure 7/16/2015. Depths lower than 235 ft not included in average since well was not at temperature when sensors failed. 7/16/2015 temperatures applied to average since well failed.

The average soil temperatures as degrees Celsius (°C) and degrees Fahrenheit (°F) are shown in the figure below by treatment zone (i.e., LSZ, UWBZ and CZ).

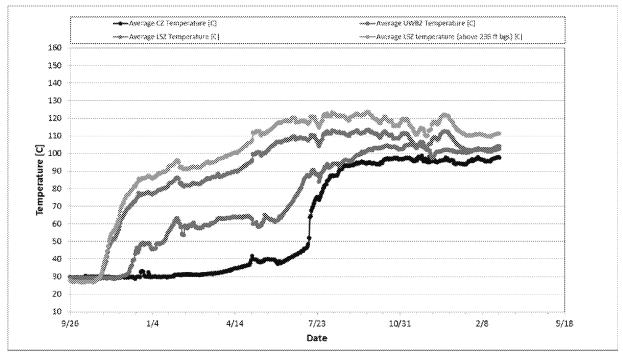


Figure 6. Average Soil Temperatures

Table 3 below provides a breakdown of the maximum average temperatures achieved at individual temperature monitoring points throughout SEE operations. The table below breaks down the average temperatures achieved across the CZ, UWBZ, Lower Permeability Zone (LPZ) and the LSZ to date. The LSZ is further broken down into the average for all LSZ sensors and those LSZ sensors above 235 ft bgs.

Table 3. Temperature Monitoring Point Maximum Depth-Averaged Temperature

•	Temperature Monitoring Point Maximum Depth-Averaged											
	Те	Temperature ¹ (°C) During SEE Operations by Zone										
Temperature					LSZ							
Monitoring Point	CZ	UWBZ	LPZ	LSZ	(depths above							
					235 ft bgs)							
TMP01	114.9	130.5	N/A	N/A	N/A							
TMP03	N/A	N/A	137.5	114.2	120.7							
TMP04	N/A	N/A	103.8	118.8	127.1							
TMP05	110.3	N/A	N/A	N/A	N/A							
TMP06	N/A	N/A	137.4	135.0	135.9							
TMP07	N/A	N/A	134.6	137.2	140.2							
TMP08	N/A	N/A	136.6	131.3	135.4							
TMP09	N/A	N/A	132.5	134.1	139.3							
TMP11	N/A	N/A	110.6	119.1	131.7							
TMP12	76.4	92.6	121.8	121.4	131.3							
TMP13	102.1	119.8	130.6	138.4	140.0							
TMP14	N/A	N/A	133.6	124.3	136.3							
TMP15	113.1	123.3	128.7	126.5	135.6							
TMP16	N/A	N/A	126.7	120.5	131.0							
TMP17	N/A	N/A	135.2	136.9	136.9							
Maximum depth-	402.2	116.6	430.4	427 F	424.0							
averaged by zone ²	103.3	116.6	128.4	127.5	134.0							

If N/A, Temperature Monitoring Point has no sensors in that zone

Temperature of the thermocouples across each depth zone are averaged for each TMP and each available time interval and then the maximum value of those averages throughout operations is listed in the table.

² Average of maximum depth-averages listed above for all TMPs in each zone.

8. Vertical and Horizontal Temperature Profiles

The following Figures 7 and 8 show the temperature in °C versus depth profiles for each of the 17 individual temperature monitoring points. Please see Table 2 for an updated temperature monitoring sensor status.

Temperature highlights for the past week include:

- Temperatures in the CZ and UWBZ at TMP 01 increased slightly. The current high temperature for this array is 128°C at the 194 ft bgs depth.
- The maximum temperature for the perimeter well TMP 02 went up slightly to 55°C. Overall the temperatures at this well remained stable.
- Slight temperature increases were observed in the UWBZ and LSZ at TMP 08.
- A slight temperature increase was observed at the 140 ft bgs sensor at perimeter well TMP 10. This well still shows a high temperature of 112°C at the 220 ft bgs depth.
- A significant temperature increase was observed in the UWBZ at TMP 11. The current high temperature for that zone is 113°C at the 170 ft bgs sensor.
- Generally all other TMPs remained stable or increased slightly.

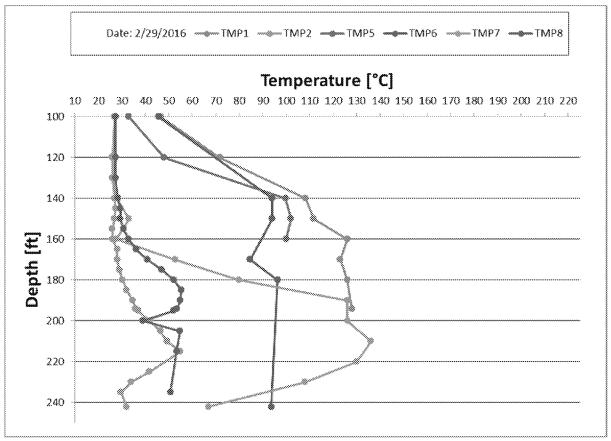


Figure 7. Vertical Temperature Profiles (TMP01 through TMP08)

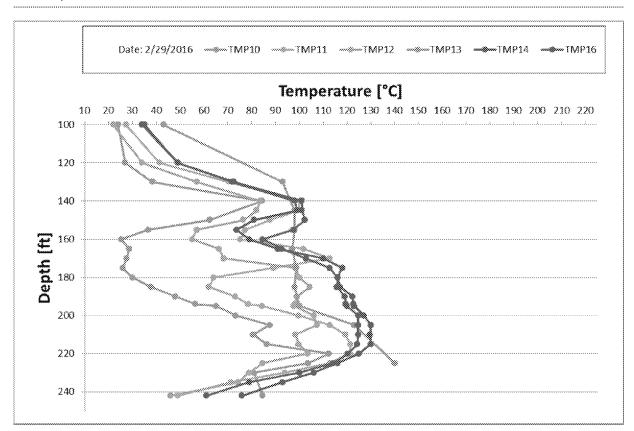


Figure 8. Vertical Temperature Profiles (TMP09 through TMP17)

Figures 9-12 show the horizontal temperature distribution across the site in four depth intervals.

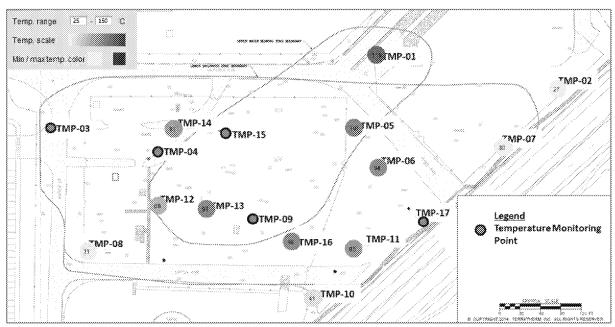


Figure 9. Horizontal Temperature Distribution across the CZ (145-160 ft bgs) (temperatures shown in °C)

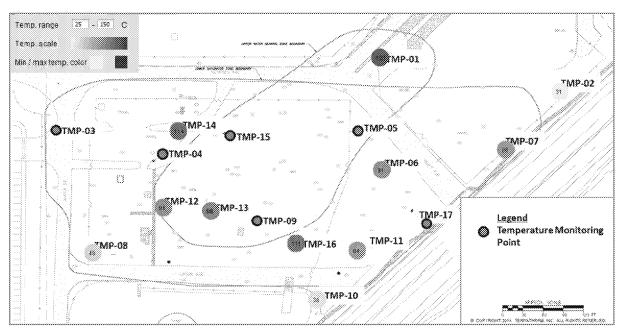


Figure 10. Horizontal Temperature Distribution across the UWBZ (161-195 ft bgs) (temperatures shown in °C)

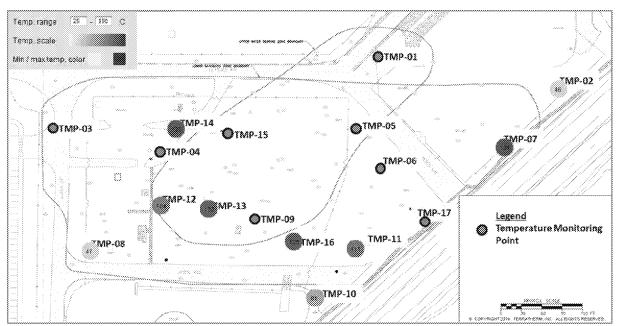


Figure 11. Horizontal Temperature Distribution across the Lower Permeable Zone (196-210 ft bgs) (temperatures shown in °C)

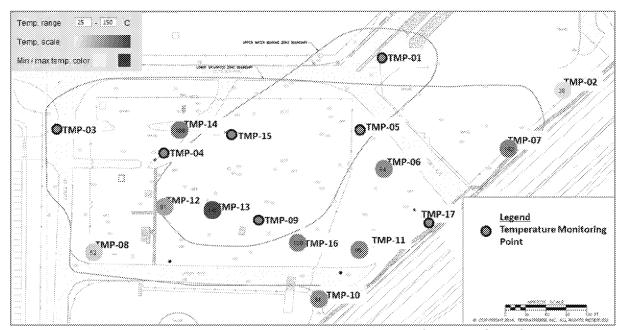


Figure 12. Horizontal Temperature Distribution across the LSZ (211-245 ft bgs) (temperatures shown in °C)

Figure 13 below shows the observed temperatures by depth at selected LSZ extraction wells.

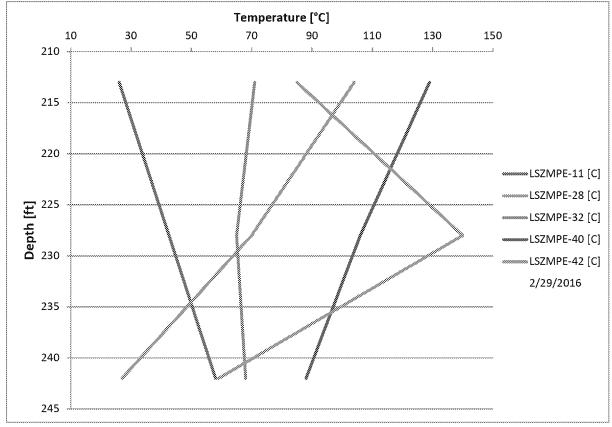


Figure 13. Temperatures by Depth at Selected LSZ Extraction Wells (211-245 ft bgs) (temperatures shown in °C)

9. Cumulative Steam Injection

Steam injection was initiated Thursday, October 16, 2014. Figure 14 below shows the cumulative steam injection for each of the three injection zones.

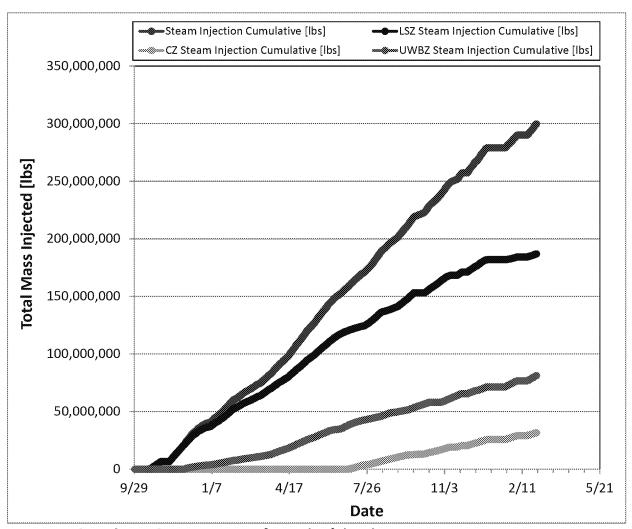


Figure 14. Cumulative Steam Injection for Each of the Three Injection Zones

10. Steam Injection Rates

The figure below shows the steam injection rates for each of the three injection zones.

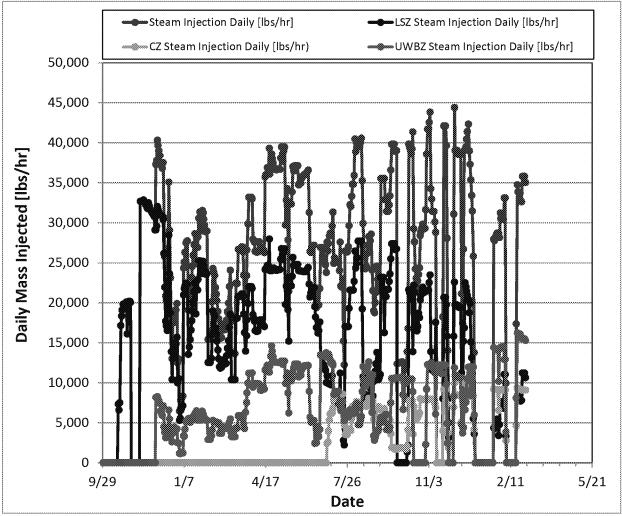


Figure 15. Steam Injection Rate for Each of the Three Injection Zones

11. Cumulative Water Extraction by Zone

The cumulative water extraction for each of the three treatment zones is shown below. The cumulative water extraction is calculated based on flow meters installed at each of the 57 extraction wells (accuracy should be considered +/- 20%). The figure below shows the net liquid extracted from the subsurface at the site and does not include the fraction of water that is recirculated to the eductor wells and used as motive water.

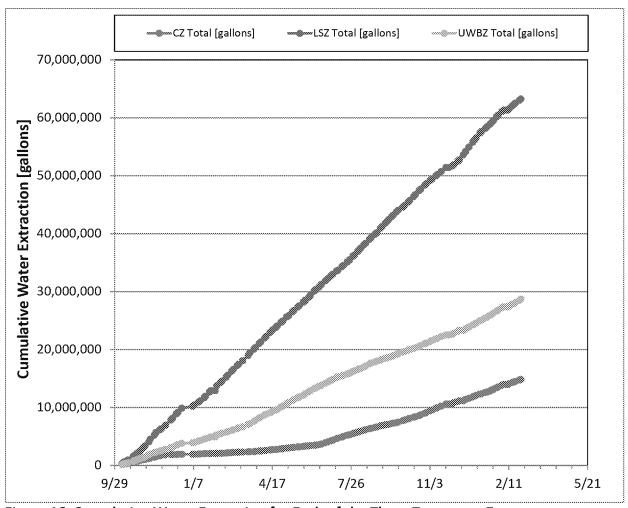


Figure 16. Cumulative Water Extraction for Each of the Three Treatment Zones

12. Water Extraction Rates by Zone

The figure below shows the water extraction rates for each of the three treatment zones.

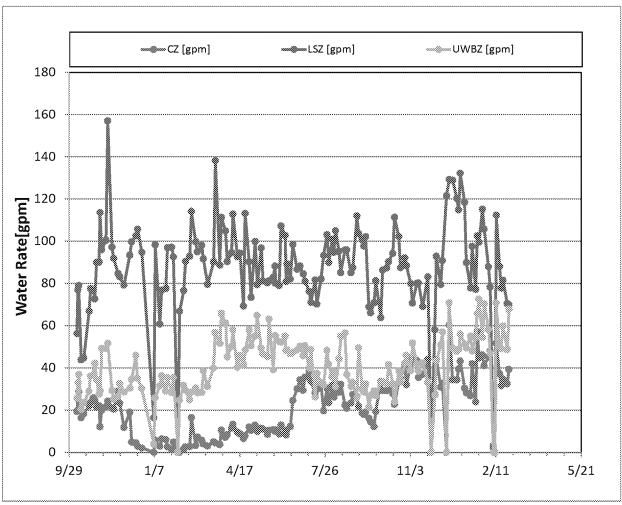


Figure 17. Water Extraction Rates for Each of the Three Treatment Zones

13. Cumulative Water Balance

The cumulative water balance for the site is shown below. The chart shows the net liquid extracted from the subsurface at the site and does not include the fraction of water that is recirculated to the eductor wells and used as motive water.

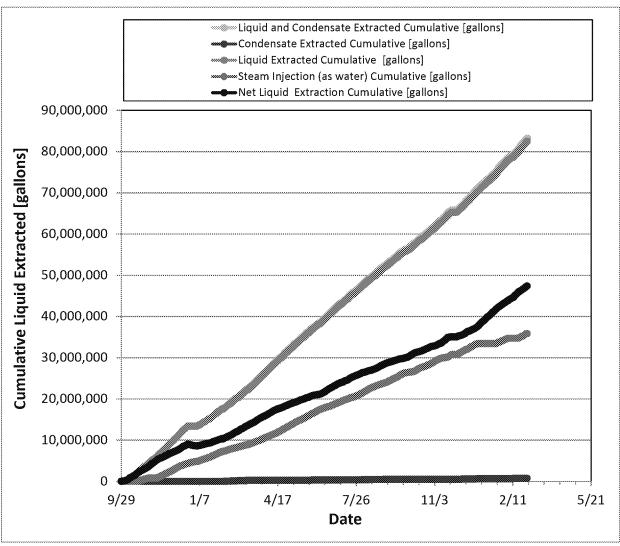


Figure 18. Cumulative Water Balance

14. Water Balance Rate

The total system water extraction rates are shown in the figure below.

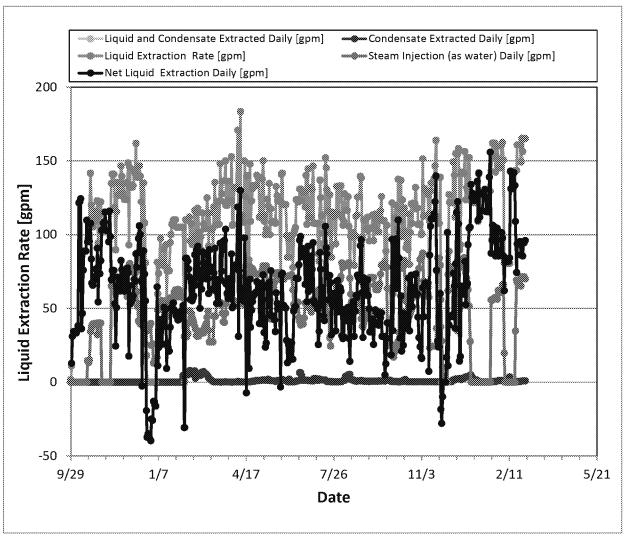


Figure 19. Water Balance Rates

15. Cumulative Energy Balance

The cumulative energy balance for the site is shown below. The energy balance has been updated to include calculated heat losses that are a combination of heat lost below the TTZ, above the TTZ and outside the TTZ. The heat losses were calculated according to the following approach:

- Based on the original SEE model, cumulative modeled heat losses were calculated for each operational phase (i.e., heat up, pressure cycling);
- The heat losses were compared to the cumulative energy added as steam for each operational phase;
- The percent of total steam energy "lost" was calculated by comparing modeled heat losses to modeled steam injection;
- Since the actual steam injection rates at ST012 have been different than originally modeled, the percent heat loss calculated for each operational phase in the model was applied to the actual steam injected to get the calculated heat losses during operation; and,
- The calculated heat losses were subtracted from the net energy injection to calculate the net energy injected with heat losses.

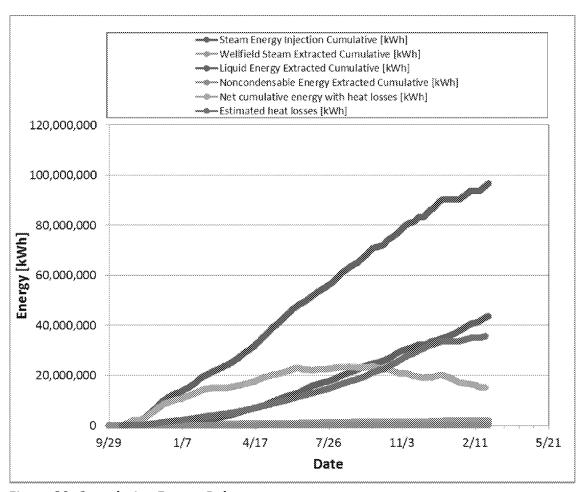


Figure 20. Cumulative Energy Balance

16. Energy Balance Rates

The energy balance rates are shown below.

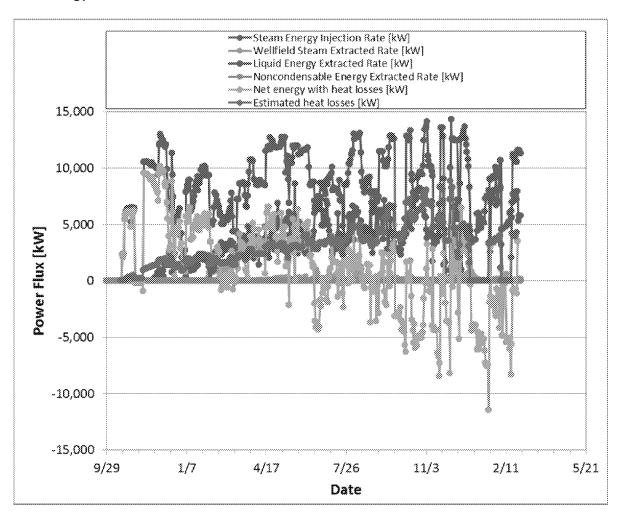


Figure 21. Energy Balance Rates

17. Perimeter Water Level Data

Table 4 below presents the change in perimeter groundwater elevations since SEE system startup. The readings collected on September 24, 2014 (not shown) represent baseline conditions. A negative number shows that the groundwater elevation is lower than the baseline elevation, thus indicating an inward hydraulic gradient into the treatment zone. Liquid extraction began on September 29, 2014. Perimeter water level data are collected on a weekly basis. The regional groundwater table at the Site is increasing at a rate of approximately 1.5 ft/year; thus, each measured value shown in Table 4 has been corrected to take the regional changes into account.

Table 4. Perimeter Groundwater Elevation Changes

	2/5/2	2016	2/12/2	2016	2/19/	2016	2/26/2016				
Monitoring Well	Change from Baseline	Change from Previous									
CZ/UWBZ Wells											
ST012-C01	-1.73	-0.10	-1.65	0.11	-1.82	-0.14	-1.73	0.12			
ST012-C02	-1.23	0.22	-1.65	-0.39	-1.96	-0.28	-1.37	0.62			
UWBZ Wells											
ST012-RB-3A	-1.24	0.31	-3.17	-1.90	-3.62	-0.42	-1.09	2.56			
ST012-U02	-1.61	-0.07	-2.55	-0.91	-2.92	-0.34	-1.11	1.84			
ST012-U11	-1.74	0.26	-3.81	-2.04	-4.15	-0.31	-1.59	2.59			
ST012-U12	-2.01	0.75	-5.00	-2.96	-5.27	-0.24	-1.40	3.90			
ST012-U37	-0.92	0.59	-4.03	-3.08	-6.31	-2.25	-0.99	5.35			
ST012-U38	-0.27	1.53	-1.98	-1.68	-0.84	1.17	-1.31	-0,44			
LSZ Wells											
ST012-W11	-4.01	0.32	-6.03	-1.99	-5.37	0.69	-3.38	2.02			
ST012-W12	-3.24	1.21	-5.14	-1.87	-5.08	0.09	-2.37	2.74			
ST012-W24	-2.67	0.59	-4.07	-1.37	-4.20	-0.10	-2.04	2.19			
ST012-W30	-2.65	0.76	-5.09	-2.41	-4.80	0.32	-2.90	1.93			
ST012-W34	-2.40	0.69	-3.76	-1.33	-3.85	-0.06	-1.77	2.11			
ST012-W36	-1.30	1.03	-3.80	-2.47	-3.65	0.18	-0.26	3.42			
ST012-W37	-4.17	0.53	-5.77	-1.58	-6.00	-0.20	-3.46	2.56			
ST012-W38	-2.23	0.57	-3.30	-1.04	-3.51	-0.18	-1.62	1.92			

Figure 22 shows the manually collected groundwater elevation trends since system startup. Additionally Figure 23 shows the groundwater elevations continuously logged in selected perimeter wells equipped with transducers. The regional groundwater table correction has also been applied to Figure 22 below.

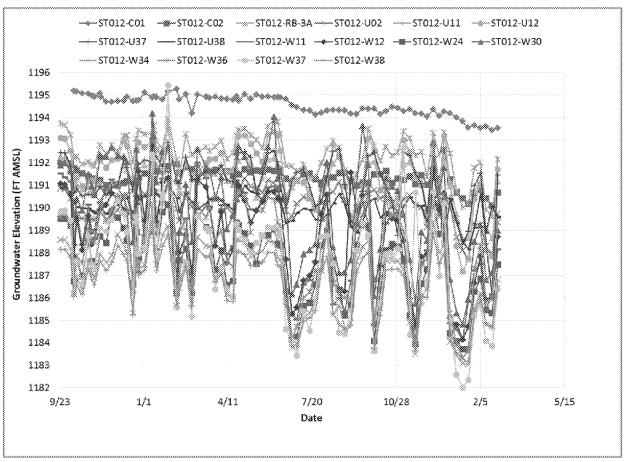


Figure 22. Manually Collected Perimeter Groundwater Elevations

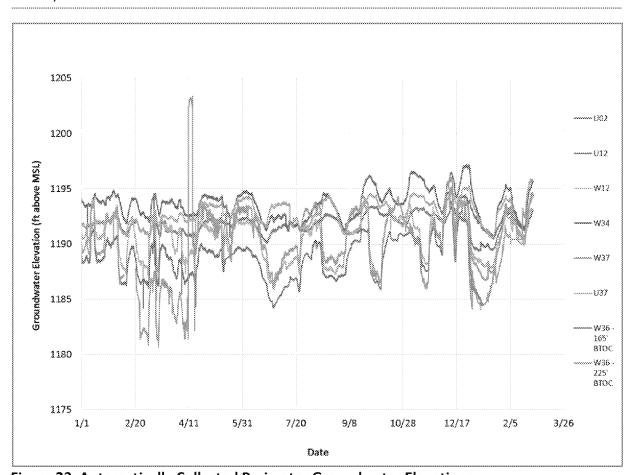


Figure 23. Automatically Collected Perimeter Groundwater Elevations

Table 5 below presents the measured LNAPL thicknesses of the perimeter wells at the site. Perimeter LNAPL thickness data are collected on a weekly basis.

Table 5. Perimeter LNAPL Thicknesses (ft)

Monitoring Well		2/5/2016			2/12/2016			2/19/2016		2/26/2016					
	Before	After	Weekly	Before	After	Weekly	Before	After	Weekly	Before	After	Weekly			
	bailing/	Bailing/	Gallons	bailing/	Bailing/	Gallons	bailing/	Bailing/	Gallons	bailing/	Bailing/	Gallons			
CZ/UWBZ Wells	pumping	pumping	Removed ¹	pumping	pumping	Removed ¹	pumping	pumping	Removed ¹	pumping	pumping	Removed ¹			
ST012-C01	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00			
ST012-C02	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00			
UWBZ Wells															
ST012-U02	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00			
ST012-U11	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00			
ST012-U12	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00			
ST012-U37	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00			
ST012-U38	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00			
ST012-RB-3A	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00			
LSZ Wells															
ST012-W11	5.49	5.49	0.00	6.01	6.01	0.00	6.06	6.06	0.00	6.87	3.66	2.00			
ST012-W12	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00			
ST012-W24	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00			
ST012-W30	0.01	0.01	0.00	0.01	0.01	0.00	0.01	0.01	0.00	0.01	0.01	0.00			
ST012-W34	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00			
ST012-W36	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00			
ST012-W37	30.87	5.62	16.48	8.99	8.99	3.58 ²	23.04	5.88	15.48 ²	28.40	1.50	17.56			
ST012-W38	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00			

Notes:

¹Estimated gallons removed based on 4-inch casing and difference in product level in well before and after removal. Does not account for volume of hose or other equipment

in the column of product. Includess all dates bailed/pumped in the week.

 $^{^2}$ In addition to the weekly measurements, ST012-W37 LNAPL levels were measured and LNAPL was pumped on 2/10/16 and 2/15/16

March 2, 2016

On December 1, 2014, temperatures at selected perimeter wells were added to the monitoring program. Figure 24 below shows the manually collected temperatures recorded at the wells included in the monitoring program. Additionally, Figure 25 shows the temperatures continuously logged in selected perimeter wells equipped with transducers.

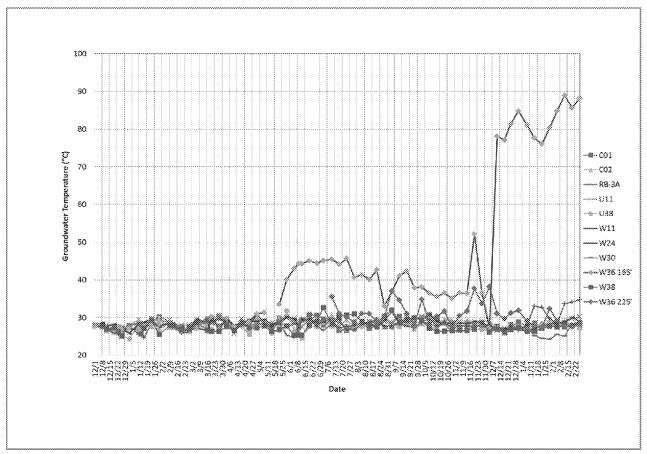


Figure 24. Manually Collected Perimeter Well Groundwater Temperatures

Note: Thermocouples are measured at approximate depths as follows (in feet below top of casing): C01=162; C02=168; RB-3A=161; U11=180; U38=164; W11=228; W24=230; W30=231; W36=225; and W38=228.

As a response to the increased temperatures observed at W36 on December 12, 2015 steam at nearby UWBZ9 and UWBZ25 were decreased.

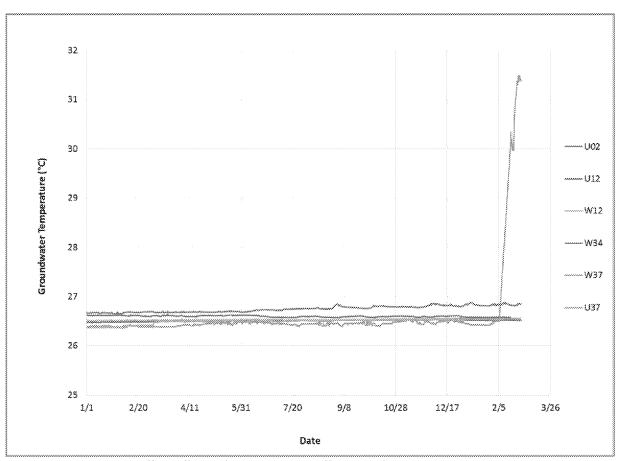


Figure 25. Automatically Collected Perimeter Well Groundwater Temperatures

Notes:

On March 7, 2015 operational personnel replaced the U37 logger unit. The increase in temperature on March 7, 2015 at U37 is a result of this replacement.

Transducers are measured at depths as follows (in feet below top of casing): U02= 175; U12= 175; U37= 182; W12= 228; W34= 225; and W37= 226.

Please note that this week's temperature data collected at W37 are suspect and currently being evaluated by field personnel.

18. Natural Gas Usage

The following figure shows the natural gas usage rate in cubic feet per hour (cf/hr) and cumulative natural gas use in cubic feet (cf) to date at the site.

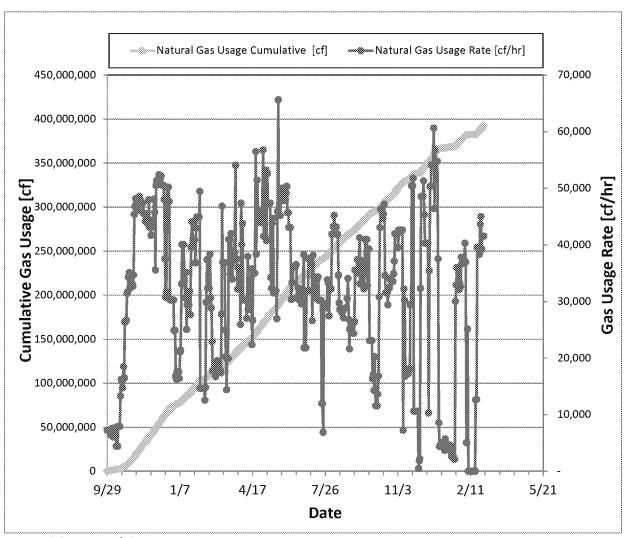


Figure 26. Natural Gas Usage

19. Waste Generation

On January 19, 2015 a total of 8,033 gallons of material from tank cleanout activities was removed from the site by Mesa Oil for recycling. The mass of JP-4 in the material was estimated to be 2,857 gallons or 18,800 lbs.

On February 18 and 19, 2015 a total of 24,430 gallons of material from tank cleanout activities was removed from the site by Mesa Oil for recycling. The mass of JP-4 in the material was estimated to be 3,645 gallons or 23,984 lbs.

On March 12, 2015 a total of 11,359 gallons of predominantly water from tank cleanout activities was removed from the site by Mesa Oil for recycling. The JP-4 mass in the water was limited.

On March 20, 2015 the first shipment of bag filters (four cubic yard boxes) from the SEE process treatment system was shipped offsite for non-hazardous disposal.

On March 30 and 31, 2015 a total of 32,000 lbs of spent liquid carbon was removed from the site by Evoqua Water Technologies for regeneration at their Red Bluff, CA facility.

On April 24, 2015 a shipment of bag filters (three cubic yard boxes) from the SEE process treatment system was shipped offsite for non-hazardous disposal.

On May 29, 2015 a shipment of bag filters (four cubic yard boxes) from the SEE process treatment system was shipped offsite for non-hazardous disposal.

On June 11, 2015 three 55-gallon drums of soil dug from around the Hypro NAPL filter were shipped offsite for non-hazardous disposal.

On June 10, 2015 a total of 5,727 gallons of oily bio-impacted water from tank cleanout activities was removed from the site by Mesa Oil for recycling.

On June 25, 2015 a shipment of bag filters (four cubic yard boxes) from the SEE process treatment system was shipped offsite for non-hazardous disposal.

On August 19, 2015 a total of 16,000 lbs of spent liquid carbon was removed from the site by Evoqua Water Technologies for regeneration at their Red Bluff, CA facility.

On August 27, 2015 a total of five totes with approximately 250 gallons each of water/solids from disinfection of the liquid carbon vessel were removed from the site by MP Environmental for disposal.

On October 22, 2015 a shipment of bag filters (four cubic yard boxes) from the SEE process treatment system was shipped offsite for non-hazardous disposal.

On November 23, 2015 a shipment of bag filters (four cubic yard boxes) from the SEE process treatment system was shipped offsite for non-hazardous disposal.

On December 31, 2015 a shipment of bag filters (four cubic yard boxes) from the SEE process treatment system was shipped offsite for non-hazardous disposal.

On February 1, 2016 a shipment of bag filters (four cubic yards) from the SEE process treatment system was shipped offsite for non-hazardous disposal.

20. NAPL Reuse

On April 7, 2015 a total of 12,647 gallons of stored NAPL was sent to Mesa Oil for reuse. The analysis showed that 703 gallons of the total fluid was water. The water has been subtracted from the NAPL recovery estimate.

On April 21-22, 2015 a total of 13,076 gallons of stored NAPL was sent to Mesa Oil for reuse. Analysis showed a water content between <1% to 3% or a total of 227 gallons of water. The water removed has been subtracted from the NAPL recovery estimate.

On May 7, 2015 a total of 5,722 gallons of stored NAPL was sent to Mesa Oil for reuse.

On May 21, 2015 a total of 1,400 gallons of stored NAPL was sent to Mesa Oil for reuse.

On June 24, 2015 a total of 6,771 gallons of stored NAPL was sent to Mesa Oil for reuse.

21. Estimated Formation Water Temperature

The estimated formation water temperatures are indicated in Table 6 below. The formation water temperatures have been estimated for each MPE well by measuring the eductor liquid feed and return flow rate together with the eductor liquid feed and return temperatures. The enthalpy increase in the liquid return temperature as compared to the liquid feed stream temperature is used to provide the MPE well specific formation temperature. Estimated formation water temperatures above the boiling point likely indicate that steam is being pulled into the liquid extraction system. These estimated data for each MPE well location are used in conjunction with the extracted vapor data collected at the MPE wells to make determinations on steam breakthrough around the site. All of these data are reviewed holistically (with other site data such as the TMP data) to determine when and where steam cycling events should commence.

The location of each MPE well is also indicated in the table. Since perimeter extraction wells are expected to extract colder water from outside of the treatment zone, the formation temperature at these locations is not expected to reach steam temperatures. Thus, full or partial steam breakthrough can still be occurring at the perimeter locations without the estimated formation water temperature being at boiling. Please note that if the estimated formation water temperature is higher than 220°C for a given well, ">220" is indicated in the table.

Please note that no vapor temperature data were collected from the MPE wellheads November 5-13, 2015 due to issues with the temperature equipment.

Table 6. Estimated Well Formation Temperatures

	MPE Formation Temperatures										MPE Forma	ation Temp	eratures													
	Well	Required to Reach	Reached Steam	Vapor Extraction	12/18/15	12/22/15	12/27/15	12/29/15	12/31/15	1/5/16	1/7/16	1/12/16	1/14/16	1/18/16	1/20/16	1/22/16	1/26/16	1/28/16	2/2/16	2/4/16	2/11/16	2/15/16	2/17/16	2/19/16	2/24/16	2/26/16
Well -	Location	Steam Temperature	Temperature (Calculated)	Max Temperature [°F]	[°F]	[°F]	[°F]	[°F]	[°F]	[°F]	[°F]	[°F]	[°F]	[°F]	[°F]	[°F]	[°F]	[°F]	[°F]	[°F]	[°F]	[°F]	[°F]	[°F]	[°F]	[°F]
CZ07	Perimeter	No	Yes	158	219	209	>220	>220	>220	205	209	206	201		202	218	155	208	>220	>220	212	104	105	100	>220	- 8
CZ08	Perimeter	No	Yes	192	215	205	>220	>220	>220	>220	201	196	172		>220	218	122						8		×220	
CZ09	Perimeter	No	Yes	105	163	126	159	124	168	131		161	147	167	197	161	107	160	123	139	76	126	>220	86	123	97
CZ10	Perimeter	No	Yes	206	199	196	181	213	199	185	186	188	198		162	176	195	196	201	>220	170	50	50	55	186	71
CZ11	Interior	Yes	Yes	217	90																					
CZ12	Perimeter	No	Yes	220						146	179	196	154	186	186	>220	136	>220	>220	>220	205	186	218	35	191	212
CZ13	Perimeter	No	Yes	160	218	>220	+220	+220	>220	>220	198	188	182		194	200	111	>220	>220	>220	83		45	80	>220	172
CZ14	Perimeter	No	Yes	112	204	+220	+220	209	204	171	131	156	150	186	177	>220	112	204	216	>220	186	96	96		>220	
CZ15	Interior	Yes	Yes	170	>220	>220	>220	+220	>220	204	208	193	191	211	182	212	102	-220	>220	>220	190	100	101	116	×220	134
CZ16	Perimeter	No	Yes	212									5220	>220	×220	>220	>220	>220	>220	>220	216	82	8.4	73	>220	>220
CZ17	Perimeter	No	Yes	200	220	214	>220	128	207	201	181	177	175	182	190	196	104	>220	>220	>220				111	209	110
CZ18	Perimeter	No	Yes	208	178	>220				>220	203					116	>220	204	>220	200	88	158	182	79	167	93
CZ19	Perimeter	No	Yes	110	5220	211			199	194	174	173	185	180	165	>220	133	209	182	>220	184	107	106	95	198	191
CZ20	Outside CZ	No	No	111	132	101	104	88	96	198			38	0	100	89	121	99	102	95	91		73	67		88
LSZ01	Interior	Yes	Yes	126	9220	159	9220	150	>220	191	209	211	152	179	193	212	181	201	206	>220	122	137	136	80	195	198
LSZ02	Interior	Yes	Yes	130	9220	>220	22.00			200	2220	157	9220	186	×220	199	182	173	181	192	74	2270	>220	316	195	66
LZS04	Interior	Yes	Yes	206																						
LSZ05	Interior	Yes	Yes	220										220	×220	>220	126	>220	>720	>220	207	149	149	130	>220	77
LSZ06	Interior	Yes	Yes	218												>220	>/20	-220	>770	>270	>220	124	124	177	207	188
LSZ08	Perimeter	No	Yes	120	ļ	151	179	179	160	133	159	113	139		143	123	105	147	155	160	138	152	143	82	130	63
LSZ11	Perimeter	No	Yes	119		113	121	101									103	102	92	96		44			94	
LSZ12	Perimeter	No	Yes	126	212	210	201	219	204	192	194	1/3	182	94	174		113	174	187	181	153	126	128	97	164	164
LSZ13	Interior	Yes	Yes	125	220	197	70	-220	>220	173	190	191	191	192	184	194	>220	193	150	167	>220	210	209	33	178	139
LSZ14	Perimeter	No	Yes	177	>220	159	>220	-220	>220	215	+220	196	189	191	191		165	199	197	196	171	125	123	68	207	169
LSZ15	Interior	Yes	Yes	208	205		>220		>220	183	>220	-220	-220	9220	>220	>220	152	>220	>220	>220		120	108	135	210	193
LSZ16	Interior	Yes	Yes	205	9220	279	>220	>220	>220	>220	178	>220	>220	220	203	208	101	>220	200	120	188	92	89	28	3.03	-
LSZ17 LSZ28	Perimeter	No No	Yes	220 129	117 9220		214 9220	124	>220	102 >220	108	97	97 >220		99 160	97 155	79 121	109	123	120 189	96 175	79 co	79 68	66	101 175	68
	Perimeter	No No	Yes		7//	180						197		2327				197	172			68		76		1
LSZ29 LSZ30	Perimeter Interior	No Yes	Yes	116 133	9220	- 180 - 220	219 +220	7220	>220 >220	214 >220	181 9220	201	218	220	195 >220	202	220	7220	194 9220	208 9 220	21.5 9220	177 9220	219	-220	9220 9220	>220
LSZ30	Interior	Yes	Yes	147	7220	-220	>220	+220 +220	>220	>220	+220	-220	>220	194	+22U +220	209	7220	207	189	+220	151	108	71		91	95
LSZ31				120	9220	9220	- 220 - 220	72.00	-220	159	96	91	187	199	191	199	156	220	216	2220 2220	3.73	76	86		91 206	186
LSZ32	Interior	Yes No	Yes Yes	130	220	9220	>220	>220	>220	437	189	>220	>220	-220	×220	122	173	>220	>220	>220		>220	9220	35	9220	
LSZ34	Perimeter Interior	Yes	Yes	168	9220	7220	>220	9220	7220 7220	220	>220	-220	194	5220	+220 +220	>220	142	114	*&&U	~2£0		74.60	7220	47	177	197 166
LSZ34 LSZ35	Perimeter	No No	Yes	121	124	135	129	136	112	128	111	111	126	108	122	recu	80	119	113	115	111	115	115	118	110	108
LSZ36	Perimeter	No	Yes	121	188	198	206	101	202	182	179	169	171	181	169		101	158	147	222	125	85	85	59	150	145
LSZ37	Perimeter	No	Yes	208		199	>220	202	6.0%	sue.	113	77	101	105	109	123	94	139	158	155	117	87	90	76	151	152
LSZ37	Perimeter	No	Yes	116	<u> </u>	149	203	188	189	152	193	158	208	>220	23/2	×220		159	>220	3.23	99	60	58	72	157	131
LSZ39	Perimeter	No	No	118	 	126	161	5.00	253.7	4.76	117	130	2,593	12	165	209	126	187	146			185	,,,,,	18	122	
LSZ40	Interior	Yes	Yes	135	>220	5220	>220	220	-220		55	92	198	91	209	>220	>220	-220	>220		>220	121		113		213
LSZ42	Perimeter	No	Yes	130		211	214		-220	>220	-220		>220	5220	+220		7220	220	-220		178	103	102	72	179	157

										ſ	VIPE Forma	ation Temp	eratures													
Well	Well	Required to Reach	Reached Steam	Vapor Extraction	12/18/15	12/22/15	12/27/15	12/29/15	12/31/15	1/5/16	1/7/16	1/12/16	1/14/16	1/18/16	1/20/16	1/22/16	1/26/16	1/28/16	2/2/16	2/4/16	2/11/16	2/15/16	2/17/16	2/19/16	2/24/16	2/26/16
wen	Location	Steam Temperature	Temperature (Calculated)	Max Temperature [°F]	[°F]	[°F]	[°F]	[°F]	[°F]	[°F]	[°F]	[°F]	[°F]	[°F]	[°F]	(°F)	[°F]	[°F]	[°F]	[°F]	[°F]	[°F]	[°F]	[°F]	[°F]	[°F]
UWBZ01	Interior	Yes	Yes	150	>220	>220	>220	>220	>220	>220	>220	>220	146	>220	>220	>220	208	-220					56	43	193	176
UWBZ02	Interior	Yes	Yes	210									86	90	91	>220	>220	+220	>220	>220		98	99	138	>220	73
UWBZ04	Interior	Yes	Yes	188	>220	>220	>220	>220	90	>220	>220	>220	>220		246	>220	124	>220	>220	>220	>220	108		101	>220	146
UWBZ05	Interior	Yes	Yes	220	178		>220									216	>220	+220	>220	>220		196		46	>220	
UWBZ06	Interior	Yes	Yes	165	128	135	132	124	111	107	115	107	109	107	101	106	115	147	164	175	169	120	119	103	165	92
UWBZ10	Perimeter	No	Yes	179	>220	>220	>220	>220	85	>220	115	>220	7		114	128	168	>220	>220	>220	186	189	161	59	>220	89
UWBZ17	Perimeter	No	Yes	220	>220	>220	>220	>220	>220	>220	>220	>220	>220		215	>220	147	>220	5220	>220	198	59	46	25	>220	63
UWBZ18	Interior	Yes	Yes	200	>220	>220	>220	>220	>220	>220	>270	>220	>220			>220	188	>220	>220	>220	>220			122	>220	95
UWBZ19	Perimeter	No	Yes	162	>220	>220	>220	>220	>220	>220	>220	>220	>220	>220	>220	>220	120	>220	>220	>230	154	121	120	69	201	98
UWBZ20	Dual Phase - Perimeter	No	No	112																					96	
UWBZ21	Outside UWBZ	No	Yes	118	194	210	>220	>220	>220	>220	>220	>220	219	196	206	202	>220	201	>220	>220	161	170	201	92	>220	>220
UWBZ22	Perimeter	No	Yes	127	187	181	>220	>220	>220	204	171	174	152	158	163	160	137	182	>/20	205	>220	23	43	>220	192	190
UWBZ23	Outside UWBZ	No	Yes	206	211	>220	>220	>220	>220	>220	>220	>220	169	212	>220	>220	>220	>220					125	38	>220	>220
UWBZ24	Dual Phase - Perimeter	No	Yes	200	-220	>220				>220	>220	>220	146	>220	-220	>220	122	2233	-220	>220	-220	218	218	91	218	>220
UWBZ26	Outside UWBZ	No	Yes	105	91								150	127	159	118	154	130	152	165		132	131		150	
UWBZ27	Outside UWBZ	No	Yes	115	126		170										163	156	200	144			52	100	166	

RED	: at or above steam temperature (≥210 °F)
GREEN	: below steam temperature (<210 °F)

22. NAPL Screening Results and Calculated Benzene Concentrations

Figures 27-29 below present the screening level results for NAPL detected in samples collected from MPE wells across the site. Screening samples are typically collected on a weekly basis. The figures below also include calculated benzene concentrations of groundwater samples collected from MPE wells across the site. Data collected prior to November 18, 2015 are not shown in the figures below.

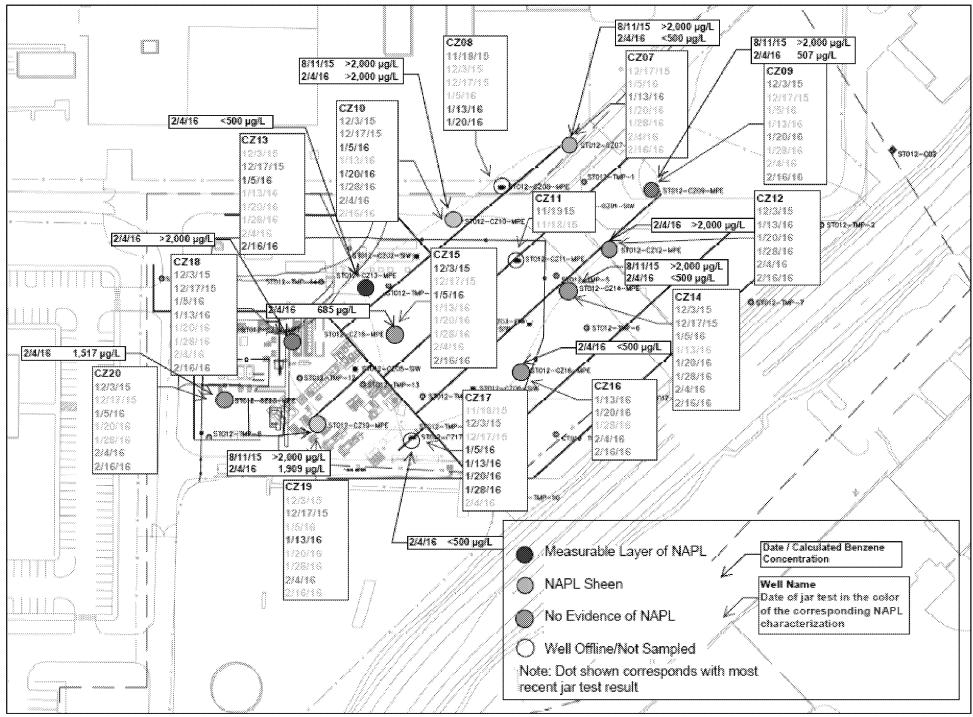


Figure 27. NAPL Screening Results and Calculated Benzene Concentrations – Cobble Zone

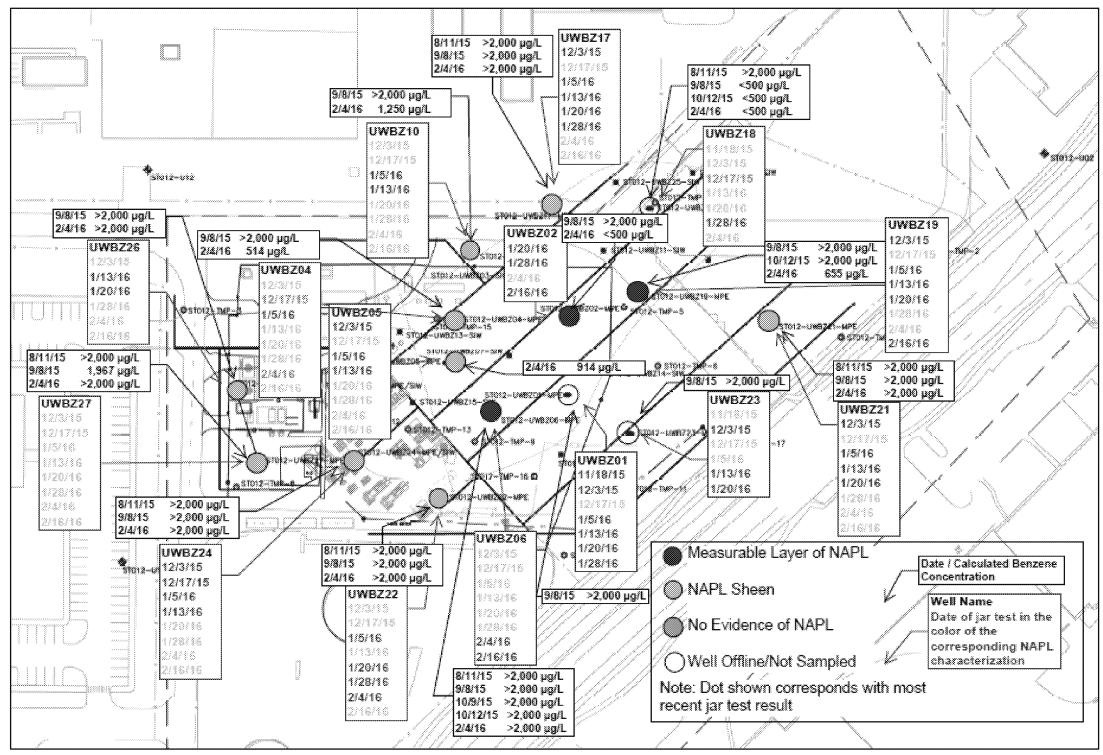


Figure 28. NAPL Screening Results and Calculated Benzene Concentrations – Upper Water Bearing Zone

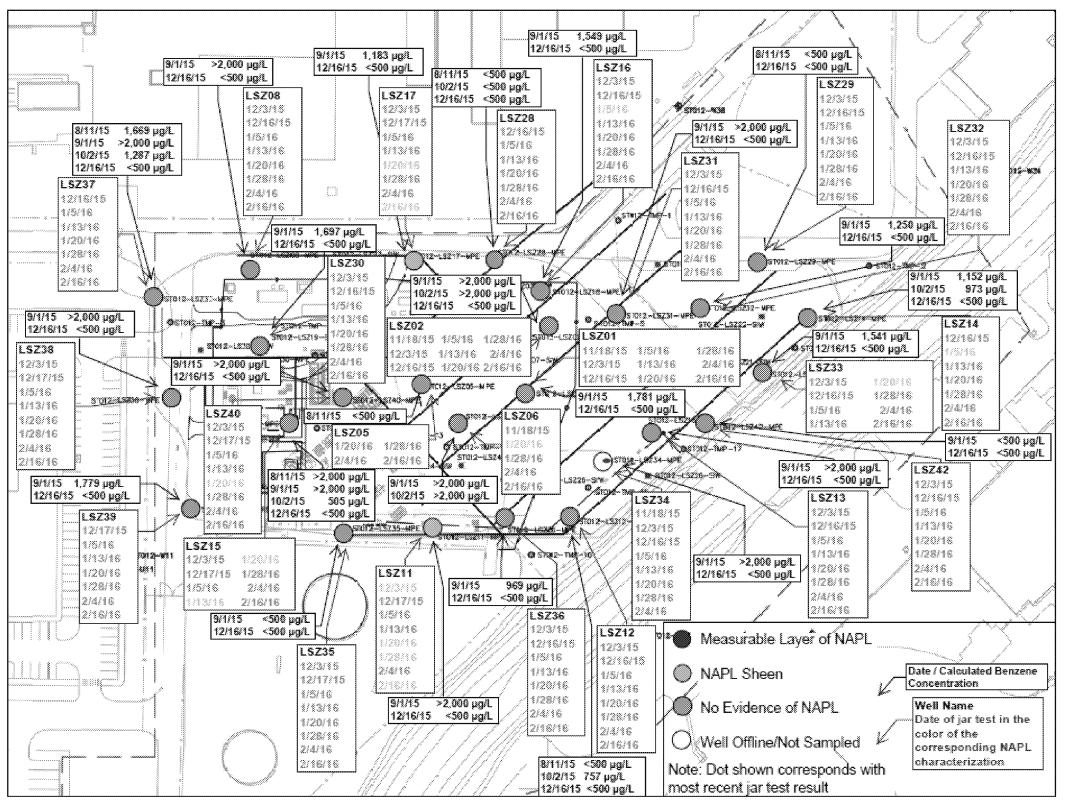


Figure 29. NAPL Screening Results and Calculated Benzene Concentrations – Lower Saturated Zone